

Final solutions (2021)

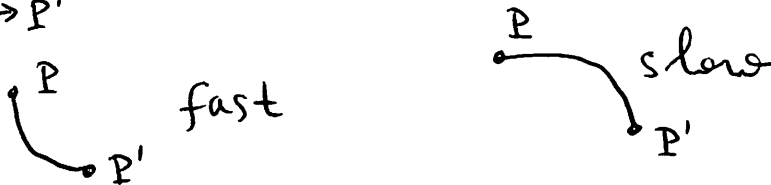
① (a) Use energy conservation:

$$T(P) = 0, \quad T(P') = \frac{m v(P')^2}{2}$$

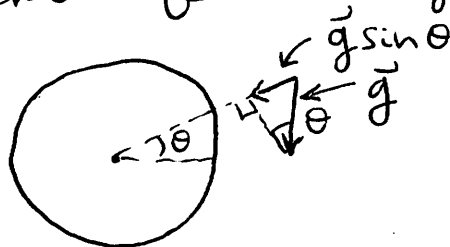
$$\frac{m v(P')^2}{2} = \frac{m g H}{3} \quad \text{gives}$$

$$v(P') = \sqrt{\frac{2}{3} g H}$$

$v(P')$ will be the same for all ramp shapes. However, we expect $t_{P \rightarrow P'}$ to depend on the ramp shape:



(b) m will leave the surface once the centrifugal force is equal to the normal component of the gravitational force:



$$\frac{m v^2}{H} = m g \sin \theta \quad (*)$$

We need to find v at the point of departure: $\frac{1}{2}v^2 = \frac{gH}{3} + g(H - H\sin\theta)$.

from $v(P')$

But $H\sin\theta = \frac{v^2}{g}$ ^(*), yielding

$$\frac{v^2}{2} = \frac{4}{3}gH - v^2,$$

$$v^2 = \frac{8}{9}gH.$$

↑
departure velocity

The height (above ground) at which it loses contact w/ the slide

is: $H + H\sin\theta = H + \frac{8}{9}H = \frac{17}{9}H$.

2.

(a) EoM:

$$\begin{cases} m_1 \ddot{x}_1 = -k_1 x_1 - k_{12}(x_1 - x_2), \\ m_2 \ddot{x}_2 = -k_{12}(x_2 - x_1) - k_2 x_2 \end{cases}$$

(b) Use $\begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} x_{1,0} \\ x_{2,0} \end{pmatrix} e^{i\omega t}$:

$$\begin{cases} (-m_1 \omega^2 + k_1 + k_{12}) x_{1,0} - k_{12} x_{2,0} = 0, \\ -k_{12} x_{1,0} + (-m_2 \omega^2 + k_2 + k_{12}) x_{2,0} = 0. \end{cases}$$

Matrix form:

$$\begin{pmatrix} \frac{k_1 + k_{12}}{m_1} - \omega^2 & -\frac{k_{12}}{m_1} \\ -\frac{k_{12}}{m_2} & \frac{k_2 + k_{12}}{m_2} - \omega^2 \end{pmatrix} \begin{pmatrix} x_{1,0} \\ x_{2,0} \end{pmatrix} = 0$$

Plug in numbers:

$$\begin{pmatrix} 8 - \omega^2 & -4 \\ -4 & 8 - \omega^2 \end{pmatrix} \begin{pmatrix} x_{1,0} \\ x_{2,0} \end{pmatrix} = 0$$

$$\det = 0 \Rightarrow (\omega^2 - 8)^2 - 16 = 0,$$

$$\omega^2 = 8 \pm 4 = \begin{cases} 12 \\ 4 \end{cases}$$

$$\text{So, } \begin{cases} \omega_1 = \sqrt{12}, & \left(\frac{\text{rad}}{\text{s}}\right) \\ \omega_2 = 2 \end{cases}$$

$$\omega_1: -4(x_{1,0} + x_{2,0}) = 0 \Rightarrow x_{1,0} = -x_{2,0}$$

$$\omega_2: 4(x_{1,0} - x_{2,0}) = 0 \Rightarrow x_{1,0} = x_{2,0}$$

(c) Use

$$\begin{cases} x_1(t) = C_1 \cos(\omega_1 t) + C_2 \cos(\omega_2 t), \\ x_2(t) = -C_1 \cos(\omega_1 t) + C_2 \cos(\omega_2 t) \end{cases}$$

↑
no initial phases since $\dot{x}_1(0) = \dot{x}_2(0) = 0$.

$$x_1(0) = 0 \Rightarrow C_1 = -C_2.$$

$$x_2(0) = 0.1 \Rightarrow 2C_2 = 0.1, \quad C_2 = 0.05 \text{ m.}$$

Finally,

$$\begin{cases} x_1(t) = -0.05 \cos(\sqrt{12}t) + 0.05 \cos(2t), \\ x_2(t) = 0.05 \cos(\sqrt{12}t) + 0.05 \cos(2t). \end{cases}$$

3. (a) Mass of liquid in the tube: $\rho a h$. Kinetic energy of the liquid:

$$T = \frac{1}{2}(\rho a h) \dot{h}^2 \quad \text{Potential energy w.r.t the reservoir: } V = \frac{1}{2} g \rho a (h-H)^2$$

$$\text{Then } \mathcal{L} = T - V = \frac{\rho a h}{2} \dot{h}^2 - \frac{g \rho a}{2} (h-H)^2$$

$$\text{next, } \begin{cases} \frac{\partial \mathcal{L}}{\partial \dot{h}} = \rho a h \dot{h}, & \Rightarrow \frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{h}} \right) = \rho a \dot{h}^2 + \rho a h \ddot{h} \\ \frac{\partial \mathcal{L}}{\partial h} = \frac{\rho a}{2} \dot{h}^2 - g \rho a (h-H) \end{cases}$$

$$\text{EoM: } h \ddot{h} + \dot{h}^2 - \frac{\dot{h}^2}{2} + g(h-H) = 0, \text{ or}$$

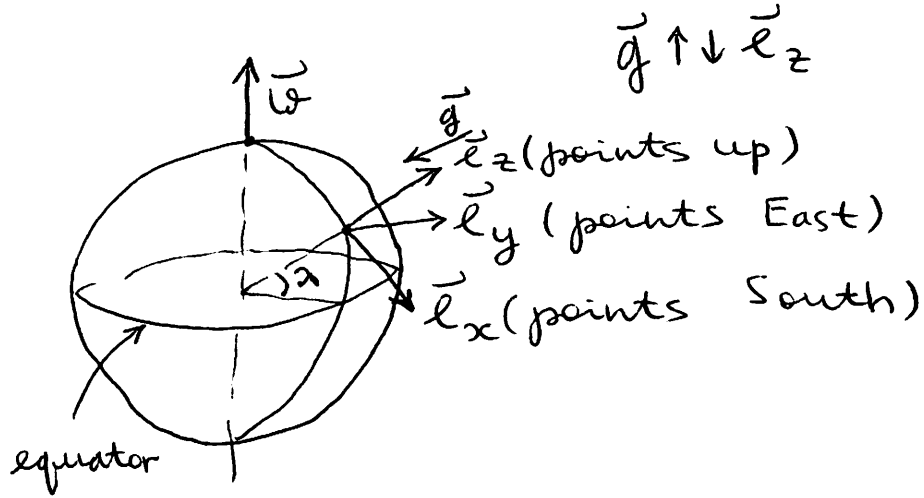
$$h \ddot{h} + \frac{\dot{h}^2}{2} + g(h-H) = 0. \quad (*)$$

(b) Eq (*) is different from the SHO eq'n: $\ddot{h} + \omega^2 (h-H) = 0$ due to the h factor in the acceler'n term and the $\frac{\dot{h}^2}{2}$ term. This is basically because the mass in the tube is not constant, and because the system is open (liquid flows out into the reservoir).

4.

$$\vec{F}_{\text{eff}} = m \underbrace{(\vec{g} - 2\vec{\omega} \times \vec{v})}_{\vec{a}}$$

Coordinate system:



$$\begin{cases} \omega_x = -\omega \cos \lambda, \\ \omega_y = 0, \\ \omega_z = \omega \sin \lambda. \end{cases}$$

To $\mathcal{O}(\omega)$, we can neglect higher-order Coriolis effects and take

$$\begin{cases} \dot{x} = 0, \\ \dot{y} = 0, \\ \dot{z} = -gt \end{cases} \quad [\text{all corrections would be } \mathcal{O}(\omega^2)]$$

$$\text{Then } \vec{\omega} \times \vec{v} = \begin{vmatrix} \vec{l}_x & \vec{l}_y & \vec{l}_z \\ -\omega \cos \lambda & 0 & \omega \sin \lambda \\ 0 & 0 & -gt \end{vmatrix} =$$

$$= -\omega g t \cos \lambda \vec{l}_y$$

Since $\vec{g} = \begin{pmatrix} 0 \\ 0 \\ -g \end{pmatrix}$,

$$\vec{a} = \begin{pmatrix} 0 \\ 2\omega g t \cos \lambda \\ -g \end{pmatrix} \leftarrow \text{Coriolis effect, force in the easterly direction}$$

So, $\ddot{y} \approx \overset{O(\omega)}{2\omega g t \cos \lambda}$.

$$y(0) = \dot{y}(0) = 0 :$$

$$y(t) = \frac{1}{3} \omega g t^3 \cos \lambda$$

Time of fall: $t \approx \sqrt{\frac{2h}{g}}$.

Finally,

$$d \approx \frac{1}{3} \omega \cos \lambda \left(\frac{2h}{g} \right)^{3/2} g = \frac{\omega \cos \lambda}{3} \left(\frac{8h^3}{g} \right)^{1/2}$$

(b) For $h = 10^2 \text{ m}$ and $\lambda = \frac{\pi}{4}$, we obtain: $d \approx \underline{\underline{1.55 \text{ cm}}}$.

5. Recall that

$$L_z = x p_y - y p_x.$$

$$\tilde{L}_z \equiv L_z$$

$$\begin{aligned} \text{Then } [u, L_z] &= \frac{\partial u}{\partial x} \frac{\partial \tilde{L}_z}{\partial p_x} + \frac{\partial u}{\partial y} \frac{\partial \tilde{L}_z}{\partial p_y} + \\ &+ \frac{\partial u}{\partial z} \frac{\partial \tilde{L}_z}{\partial p_z} - \frac{\partial u}{\partial p_x} \frac{\partial \tilde{L}_z}{\partial x} - \frac{\partial u}{\partial p_y} \frac{\partial \tilde{L}_z}{\partial y} - \\ &- \frac{\partial u}{\partial p_z} \frac{\partial \tilde{L}_z}{\partial z} = \frac{\partial u}{\partial x} (-y) + \frac{\partial u}{\partial y} x - \\ &- \frac{\partial u}{\partial p_x} p_y - \frac{\partial u}{\partial p_y} (-p_x). \end{aligned}$$

$$\begin{aligned} \text{Now, } \frac{\partial u}{\partial x} &= \frac{\partial u}{\partial r^2} \frac{dr^2}{dx} + \frac{\partial u}{\partial (\vec{r} \cdot \vec{p})} \frac{d(\vec{r} \cdot \vec{p})}{dx} = \\ &= u' \times (2x) + \tilde{u}' p_x, \text{ etc.} \end{aligned}$$

$$\begin{aligned} \text{Then } [u, L_z] &= (-2xy) u' - y p_x \tilde{u}' + \\ &+ (2xy) u' + p_y x \tilde{u}' - [u' \times (2p_x) + \tilde{u}' x] p_y + \\ &+ [u' \times (2p_y) + \tilde{u}' y] p_x = \tilde{u}' [-y p_x + p_y x - x p_y + \\ &+ y p_x] = \underline{\underline{0}}, \text{ as desired.} \end{aligned}$$