

For the TE modes,

$$\begin{aligned}\frac{C}{A}\zeta_{mn}^{\text{TE}} &= \int_{\Gamma} |\hat{n} \times \nabla_t \psi|^2 \Big/ (\gamma_{mn}^{\text{TE}})^2 \int_A \psi^2 \\ &= \frac{m^2 \pi J_m^2(x'_{mn})/r}{\pi (\gamma_{mn}^{\text{TE}})^2 r^2 \frac{1}{2} (1 - (m/(x'_{mn}))^2) J_m^2(x'_{mn})} \\ &= \frac{2m^2}{r(x_{mn}'^2 - m^2)}.\end{aligned}$$

$$\begin{aligned}\frac{C}{A}\zeta_{mn}^{\text{TE}} &= \int_{\Gamma} |\psi|^2 \Big/ \int_A \psi^2 = \frac{\pi r J_m^2(x'_{mn})}{\frac{\pi}{2} (1 - (m/(x'_{mn}))^2) J_m^2(x'_{mn})} \\ &= \frac{2x_{mn}'^2}{r(x_{mn}'^2 - m^2)}.\end{aligned}$$

So the attenuation coefficient is

$$\beta_{mn}^{\text{TE}} = \sqrt{\frac{\epsilon}{\mu}} \frac{1}{r \sigma \delta_{\lambda}} \frac{\sqrt{\omega/\omega_{\lambda}}}{\sqrt{1 - \frac{\omega_{\lambda}^2}{\omega^2}}} \left[\frac{1}{(x_{mn}'^2 - m^2)} + \left(\frac{\omega_{\lambda}}{\omega} \right)^2 \right].$$

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For TM modes, $\omega_{mn}^{\text{TM}} = x_{mn} c/r$.

For copper, the resistivity is $\rho = \sigma^{-1} = 1.7 \times 10^{-8} \Omega \cdot \text{m}$.

Take $\mu_c = \mu_0$. Also $\omega_{\lambda} = \gamma_{\lambda} c$. $\delta_{\lambda} = \sqrt{2/\mu_c \sigma \omega_{\lambda}}$.

$\epsilon_0 = 8.854 \times 10^{-12} \text{C}^2/\text{N} \cdot \text{m}^2$, so

$$\begin{aligned}\sqrt{\frac{\epsilon}{\mu}} \frac{1}{\sigma \delta_{\lambda}} &= \sqrt{\frac{c \epsilon_0 \gamma_{\lambda}}{2 \sigma}} = 4.75 \times 10^{-6} \sqrt{\gamma_{\lambda}} \sqrt{\frac{\text{m}}{\text{s}} \frac{\text{C}^2}{\text{N} \cdot \text{m}^2} \Omega \text{m}} \\ &= 4.75 \times 10^{-6} \text{m}^{1/2} \cdot \sqrt{\frac{x_{mn}}{r}}.\end{aligned}$$

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The units combine to $\text{m}^{1/2}$ as $\Omega = \frac{V}{A} = \frac{J/C}{C/s} = \text{Nms}/\text{C}^2$.

In comparison to the TM_{12} mode for a square of side a , we see that $\beta^{\text{TM}} = \frac{a}{2r} \beta_{12}^{\text{TM}}$. As the cutoff frequencies are $2.4048c/r$ and $\sqrt{5}\pi c/a$ respectively, we see that the comparable dimensions are $r = (2.4048/\sqrt{5}\pi)a = 0.342a$, much smaller, and then $a/2r = 1.46$, so the smaller pipe does have faster attenuation.

Resonant Cavities

In infinite cylindrical waveguide, have waves with (angular) frequency ω for each arbitrary definite wavenumber k , with $\omega = c\sqrt{k^2 + \gamma_{\lambda}^2}$. For each mode λ and each $\omega > \omega_{\lambda} = c\gamma_{\lambda}$, there are two modes,

$k = \pm \sqrt{\omega^2/c^2 - \gamma_{\lambda}^2}$.

Standing waves by superposition.

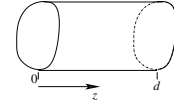
Flat conductors at $z=0$ and $z=d$.

For TM, the determining field is

$$E_z = \left(\psi^{(k)} e^{ikz} + \psi^{(-k)} e^{-ikz} \right) e^{-i\omega t},$$

$$\vec{E}_t = i \frac{k}{\gamma_{\lambda}} \vec{\nabla}_t \psi^{(k)} e^{ikz} + i \frac{-k}{\gamma_{\lambda}} \vec{\nabla}_t \psi^{(-k)} e^{-ikz}$$

$\vec{E}_t = 0$ at endcap so $\psi^{(k)} = \psi^{(-k)}$ (at $z=0$) and $\sin kd = 0$ (at $z=d$). So $k = p\pi/d$, $p \in \mathbb{Z}$.



For TE modes, there is an extra factor of

$$\frac{1}{(x_{mn}'^2 - m^2)} + \left(\frac{\omega_{\lambda}}{\omega} \right)^2.$$

which for the lowest mode is $0.4185 + (\omega_{\lambda}/\omega)^2$ compared to $0.5 + (\omega_{\lambda}/\omega)^2$ for the square. But the cutoff frequencies are now $1.841c/r$ and $\sqrt{2}\pi c/a$, so comparable dimensions have $r = 1.841a/\sqrt{2}\pi = 0.414a$.

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Thus the TM fields are

$$\left. \begin{aligned} E_z &= \cos\left(\frac{p\pi z}{d}\right) \psi(x, y) \\ \vec{E}_t &= -\frac{p\pi}{d\gamma_{\lambda}^2} \sin\left(\frac{p\pi z}{d}\right) \vec{\nabla}_t \psi \\ \vec{H}_t &= i \frac{\epsilon \omega}{\gamma_{\lambda}^2} \cos\left(\frac{p\pi z}{d}\right) \hat{z} \times \vec{\nabla}_t \psi \end{aligned} \right\} \begin{cases} \text{for TM modes} \\ \text{with } p \in \mathbb{Z} \end{cases}$$

Note that in choosing signs we must keep track that half the wave has wavenumber $-k$.

For TE modes, H_z determines all, and must vanish at endcaps (as $\hat{n} \cdot \vec{B}$ vanishes at boundaries). So

$$\left. \begin{aligned} H_z &= \sin\left(\frac{p\pi z}{d}\right) \psi(x, y) \\ \vec{H}_t &= \frac{p\pi}{d\gamma_{\lambda}^2} \cos\left(\frac{p\pi z}{d}\right) \vec{\nabla}_t \psi \\ \vec{E}_t &= -i \frac{\omega \mu}{\gamma_{\lambda}^2} \sin\left(\frac{p\pi z}{d}\right) \hat{z} \times \vec{\nabla}_t \psi \end{aligned} \right\} \begin{cases} \text{for TE modes} \\ \text{with } p \in \mathbb{Z}, p \neq 0. \end{cases}$$

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Generally the 2D mode λ requires two indices.

For a circular cylinder, we have angular index m ,

and radial index n specifying which root of J_m (for TM) or of $dJ(x)/dx$ (for TE).

$$\gamma_{mn} = \begin{cases} x_{mn}/R & \text{(TM modes)} & J_m(x_{mn}) = 0 \\ x'_{mn}/R & \text{(TE modes)} & \frac{dJ_m}{dx}(x'_{mn}) = 0 \end{cases}.$$

with R the radius of the cylinder.

Now we have a third index, p .

$$\begin{aligned}\omega_{mnp} &= \frac{1}{\sqrt{\mu \epsilon}} \sqrt{\frac{x_{mn}^2}{R^2} + \frac{p^2 \pi^2}{d^2}} & \text{with } p \geq 0 \text{ for TM modes,} \\ \omega_{mnp} &= \frac{1}{\sqrt{\mu \epsilon}} \sqrt{\frac{x_{mn}'^2}{R^2} + \frac{p^2 \pi^2}{d^2}} & \text{with } p > 0 \text{ for TE modes.}\end{aligned}$$

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Lowest TM mode, $\omega_{010} = cx_{01}/R = 2.405c/R$, independent of d .

For TE modes, $p \neq 0$, so lowest mode with $\gamma = x'_{11}/R$ has

$$\omega_{111} = 1.841 \frac{c}{R} \sqrt{1 + 2.912 R^2 / d^2}.$$

As this depends on d , such a cavity can be tuned by having a movable piston for one endcap.

Power Loss and Quality Factor

What if conductor not perfect? Power losses in sides and in endcaps. Rate is proportional to $U(t)$, the energy stored inside. Let

$$-\Delta U = \text{energy loss per cycle}, \quad Q := 2\pi U/|\Delta U|.$$

One period is $\Delta t = 2\pi/\omega$. Assume $Q \gg 1$, so $|\Delta U| \ll U$, $\Delta U = -2\pi U/Q = (2\pi/\omega)dU/dt$, so

$$U(t) = U(0)e^{-\omega t/Q}.$$

Q is called the resonance “quality factor” or “Q-value”. So if an oscillation excited at time $t = 0$ by momentary external influence,

$$U(t) \propto e^{-\omega t/Q} \implies E(t) = E_0 e^{-i\omega_0(1-i/2Q)t} \Theta(t),$$

The Heaviside function $\Theta(t) = 1$ for $t > 0$, $= 0$ for $t < 0$. This $\delta(t)$ excitation consists of equal amounts at all frequencies.

Breit-Wigner

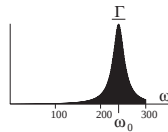
It produces a frequency response

$$\begin{aligned} E(\omega) &= \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} E(t) e^{i\omega t} dt \\ &= \frac{1}{\sqrt{2\pi}} E_0 \int_0^{\infty} e^{i(\omega - \omega_0 - i\Gamma/2)t} dt \\ &= \frac{iE_0}{\sqrt{2\pi}} \frac{1}{\omega - \omega_0 - i\Gamma/2}, \end{aligned}$$

with $\Gamma := \omega_0/Q$.

$|E(\omega)|^2$ gives the response to excitations of any frequency, with

$$|E(\omega)|^2 \propto \frac{1}{(\omega - \omega_0)^2 + \Gamma^2/4}.$$



This is called the Breit-Wigner response. Γ is mistakenly called the half-width. Really full-width at half-maximum.

Calculation of power loss as for waveguide, but need to include power loss in endcaps as well. Jackson, pp 373-374. We will skip this.

Earth and Ionosphere:

Not all cavities cylindrical. Consider surface of Earth, and ionosphere, an ionized layer about 100 km up. Concentric conducting spheres acting as endcaps, of a waveguide with no walls, but topology!

Need spherical coordinates, of course. More generally, may need other curvilinear coordinates (as you will for your projects).

So we will digress to discuss curvilinear coordinates.