## Physics 504, Spring 2010 **Electricity and Magnetism**

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#### **Course Information**

- ► Instructor:
  - ▶ Joel Shapiro
  - ► Serin 325
  - 5-5500 X 3886, shapiro@physics
- ▶ Book: Jackson: Classical Electrodynamics (3rd Ed.)
- ► Web home page: www.physics.rutgers.edu/grad/504 contains general info, syllabus, lecture and other notes, homework assignments, etc.
- ▶ Classes: ARC 207, Monday and Thursday, 10:20 (sharp!) - 11:40
- ▶ Homework: there will be one or two projects, and homework assignments every week or so. Due dates to be discussed.
- Exams: a midterm and a final.
- ▶ Office Hour: Tuesdays, 3:30–4:30, in Serin 325.

#### **Course Content**

Last term you covered Jackson, Chapters 1—7 We will cover most of chapters 8—16

Everything comes from Maxwell's Equations and the Lorentz Force. We will discuss:

- ▶ EM fields confined: waveguides, cavities, optical fibers
- ▶ Sources of fields: antennas and their radiation, scattering and diffraction
- ▶ Relativity, and relativistic formalism for E&M
- ▶ Relativistic particles
- $\blacktriangleright$  other gauge theories

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### Maxwell's Equations

 $\vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon_0} \rho_{\rm all}$  Gauss for E  $\vec{\nabla} \cdot \vec{B} = 0$  Gauss for B  $\vec{\nabla} \times \vec{B} - \frac{1}{c^2} \frac{\partial \vec{E}}{\partial \vec{d}} = \mu_0 \vec{J}_{\rm all}$  Ampère (+M Ampère (+Max)  $\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0$ Faraday

plus the Lorentz force:

 $\vec{F} = a(\vec{E} + \vec{v} \times \vec{B})$ 

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#### In "Ponderable Media"

In the last slide,  $\rho_{\rm all}$  and  $\vec{J}_{\rm all}$  represent all charges, both "free" and "induced".

Separate "free" from "induced":

- ▶ For the electric field
  - $ightharpoonup \vec{E}$  called electric field
  - $\blacktriangleright$   $\vec{P}$  called  $electric\ polarization$  is induced field
  - $ightharpoonup \vec{D}$  called electric displacement is field of "free charges"
  - $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$
- $\blacktriangleright$  For the magnetic field
  - $ightharpoonup \vec{B}$  called magnetic induction (unfortunately)
  - $ightharpoonup \vec{M}$  called magnetization is the induced field
  - ►  $\vec{H}$  called magnetic field ►  $\vec{H} = \frac{1}{\mu_0} \vec{B} \vec{M}$

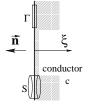
Then the two Maxwell equations with sources, Gauss for  $\vec{E}$  and Ampère, get replaced by

$$\vec{\nabla} \cdot \vec{D} = \rho$$

$$\vec{\nabla} \times \vec{H} - \frac{\partial \vec{D}}{\partial t} = \vec{J}$$

## Interface between conductor and non-conductor

Conductor c: if perfect, no  $\vec{E}$ . Surface charge  $\Sigma$ , eddy currents so no  $\vec{H}$  inside conductor. Just outside the conductor: Faraday on loop  $\Gamma \longrightarrow E_{\parallel} \approx 0$ Gauss on pillbox  $S \longrightarrow B_{\perp} \approx 0$ 



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For good (not perfect) conductor, take  $\vec{J} = \sigma \vec{E}$  with large conductivity  $\sigma$ . Assume time-dependence  $\propto e^{-i\omega t}$ Skin depth  $\xi$ ,  $\vec{H}$  varies rapidly.

$$\vec{\nabla} \times \vec{H}_c = \vec{J} + \frac{\partial \vec{D}}{\partial t} \approx \sigma \vec{E},$$

$$\vec{\nabla} \times \vec{E_c} = -\frac{\partial \vec{B}}{\partial t} = i \omega \mu_c H_c$$

Rapid variation with depth  $\xi$  dominates,  $\vec{\nabla} = -\hat{n}\frac{\partial}{\partial \xi}$ , and

$$\vec{E}_c = \frac{1}{\sigma} \vec{J} = -\frac{1}{\sigma} \hat{n} \times \frac{\partial \vec{H}_c}{\partial \xi}, \qquad \vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi}$$

$$\vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi}$$

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From  $\vec{H}_c = \vec{H}_{\parallel} e^{-\xi/\delta} e^{i\xi/\delta}$ .

$$\vec{E_c} = -\frac{1}{\sigma}\hat{n}\times\frac{\partial\vec{H_c}}{\partial\xi} = \sqrt{\frac{\mu_c\omega}{2\sigma}}(1-i)\hat{n}\times\vec{H}_{\parallel}e^{-\xi/\delta}e^{i\xi/\delta},$$

which means, by continuity, that just outside the conductor

$$\vec{E}_{\parallel} = \sqrt{\frac{\mu_c \omega}{2\sigma}} (1 - i) \hat{n} \times \vec{H}_{\parallel}.$$

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In terms of surface current

$$\begin{split} \vec{K}_{\text{eff}} &= \int_0^\infty d\xi \, \vec{J}(\xi) = \frac{1}{\delta} \hat{n} \times \vec{H}_{\parallel} \int_0^\infty d\xi \, (1-i) e^{-\xi(1-i)/\delta} \\ &= \hat{n} \times \vec{H}_{\parallel}. \end{split}$$

Thus

$$\frac{dP_{\rm loss}}{dA} = \frac{1}{2\sigma\delta} |\vec{K}_{\rm eff}|^2. \label{eq:loss}$$

 $\frac{1}{\sigma\delta}$  is surface resistance (per unit area) and  $\frac{\vec{E}_{||}}{\vec{K}_{\rm off}} = \frac{1-i}{\sigma\delta}$ is the surface impediance Z.

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 $\vec{E}_c = \frac{1}{\sigma} \vec{J} = -\frac{1}{\sigma} \hat{n} \times \frac{\partial \vec{H}_c}{\partial \xi}, \qquad \vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi}$ 

$$\begin{split} \hat{n} \times \vec{H}_c &= \frac{i}{\omega \mu_c} \hat{n} \times \left( \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi} \right) \\ &= -\frac{i}{\sigma \omega \mu_c} \hat{n} \times \left( \hat{n} \times \left[ \hat{n} \times \frac{\partial^2 \vec{H}_c}{\partial \xi^2} \right] \right) \\ &= \frac{i}{\sigma \omega \mu_c} \frac{\partial^2}{\partial \xi^2} \left( \hat{n} \times \vec{H}_c \right). \end{split}$$

Simple DEQ, exponential solution, with  $\delta = \sqrt{\frac{2}{u \omega \sigma}}$ .

$$\vec{H}_c = \vec{H}_{\parallel} e^{-\xi/\delta} e^{i\xi/\delta},$$

 $H_{\parallel}$  is tangential field outside surface of conductor.

How much power is dissipated (per unit area?). 2 ways: 1) Flow of energy into conductor: Energy flow given by  $\vec{S} = \vec{E} \times \vec{H}$ , for real fields  $\vec{E}$  and  $\vec{H}$ .

so<sup>1</sup> 
$$\langle \vec{S} \rangle = \frac{1}{2} \text{Re} \left( \vec{E} \times \vec{H}^* \right)$$

$$\begin{split} \frac{dP_{\rm loss}}{dA} &= -\hat{n} \cdot \langle \vec{S} \rangle \\ &= -\frac{1}{2} \sqrt{\frac{\mu_c \omega}{2\sigma}} \hat{n} \cdot \text{Re} \left[ (1-i)(\hat{n} \times \vec{H}_{\parallel}) \times \vec{H}_{\parallel}^* \right] \\ &= \frac{\mu_c \omega \delta}{4} |\vec{H}_{\parallel}|^2 = \frac{1}{2\sigma \delta} |\vec{H}_{\parallel}|^2 \end{split}$$

Method 2, Ohmic heating, power lost per unit volume  $\frac{1}{2}\vec{J}\cdot\vec{E}^*=|\vec{J}|^2/2\sigma, |\vec{J}|=\sigma\vec{E}_c=\frac{\sqrt{2}}{\delta}|\vec{H}_{\parallel}|e^{-\xi/\delta},$  the power loss per unit area is

$$\frac{dP_{\text{loss}}}{dA} = \frac{1}{\delta^2 \sigma} |\vec{H}_{\parallel}|^2 \int_0^{\infty} d\xi \, e^{-2\xi/\delta} = \frac{1}{2\delta \sigma} |\vec{H}_{\parallel}|^2.$$

Agrees with method 1.

The  $\frac{1}{2}$ , Re, and \* will be discussed indecture 3.  $\rightarrow$   $\rightarrow$   $\rightarrow$   $\rightarrow$   $\rightarrow$   $\rightarrow$ 

#### Wave Guides

For electromagnetic fields with a fixed geometry of linear materials, fourier transform decouples, and we can work with frequency modes,

$$\vec{E}(\vec{x},t) = \vec{E}(x,y,z) e^{-i\omega t}$$
  
 $\vec{B}(\vec{x},t) = \vec{B}(x,y,z) e^{-i\omega t}$ 

Actually the fields are the real parts of these complex

If  $\rho = 0$ ,  $\vec{J} = 0$ , Maxwell gives

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = i\omega \vec{B}, \qquad \vec{\nabla} \cdot \vec{E} = 0, \qquad \vec{\nabla} \cdot \vec{B} = 0,$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{\nabla} \times \vec{H} = \mu \frac{\partial \vec{D}}{\partial t} = \mu \epsilon \frac{\partial \vec{E}}{\partial t} = -i\omega \mu \epsilon \vec{E}.$$

$$\nabla^2 \vec{E} = -\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) + \vec{\nabla} \left( \vec{\nabla} \cdot \vec{E} \right) = -\vec{\nabla} \times (i\omega \vec{B}) = -\omega^2 \mu \epsilon \vec{E}.$$

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and similarly for  $\vec{B}$ , so we get Helmholtz equations

$$(\nabla^2 + \omega^2 \mu \epsilon) \vec{E} = 0, \qquad (\nabla^2 + \omega^2 \mu \epsilon) \vec{B} = 0.$$

Consider a waveguide, a cylinder of arbitrary cross section but uniform in z. Fourier transform in z

$$\vec{E}(x, y, z, t) = \vec{E}(x, y)e^{ikz-i\omega t}$$
  
 $\vec{B}(x, y, z, t) = \vec{B}(x, y)e^{ikz-i\omega t}$ 

k can take either sign (and a standing wave is a superposition of  $k = \pm |k|$ ). The Helmholtz equations give

$$\left[\nabla_t^2 + (\mu\epsilon\omega^2 - k^2)\right] \begin{pmatrix} \vec{E}(x,y) \\ \vec{B}(x,y) \end{pmatrix} = 0, \quad \nabla_t^2 := \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}.$$



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### Decompose longitudinal and transverse

Let

$$ec{E} = E_z \hat{z} + ec{E}_t$$
 with  $ec{E}_t \perp \hat{z}$   
 $ec{B} = B_z \hat{z} + ec{B}_t$   $ec{B}_t \perp \hat{z}$ 

$$\begin{split} (\vec{\nabla}\times\vec{E})_z &= (\vec{\nabla}_t\times\vec{E}_t)_z = i\omega B_z, \\ (\vec{\nabla}\times\vec{E})_\perp &= \hat{z}\times\frac{\partial\vec{E}_t}{\partial z} - \hat{z}\times\nabla_t E_z = i\omega\vec{B}_t. \end{split}$$

For any vector  $\vec{V}$ ,  $\hat{z} \times (\hat{z} \times \vec{V}) = -\vec{V} + \hat{z}(\hat{z} \cdot V)$ , so for a transverse vector  $\hat{z} \times (\hat{z} \times \vec{V}_t) = -\vec{V}_t$ . Taking  $\hat{z} \times$  last equation,

$$\frac{\partial \vec{E}_t}{\partial z} - \vec{\nabla}_t E_z = -i\omega \hat{z} \times \vec{B}_t. \tag{1}$$

Similarly decomposition of  $\vec{\nabla} \times \vec{B} = -i\omega\mu\epsilon\vec{E}$  gives

$$\left(\vec{\nabla}_t \times \vec{B}_t\right)_z = -i\omega\mu\epsilon E_z$$

$$\frac{\partial \vec{B}_t}{\partial z} - \vec{\nabla}_t B_z = i\omega\mu\epsilon \hat{z} \times \vec{E}_t.$$
(2)

Divergencelessness:

$$\vec{\nabla}_t \cdot \vec{E}_t + \frac{\partial E_z}{\partial z} = 0, \qquad \vec{\nabla}_t \cdot \vec{B}_t + \frac{\partial B_z}{\partial z} = 0.$$

Equations (1) and (2), with the fourier transform in z, give

$$ik\vec{E}_t + i\omega\hat{z} \times \vec{B}_t = \vec{\nabla}_t E_z \tag{3}$$

$$ik\vec{B}_t - i\omega\mu\epsilon\hat{z} \times \vec{E}_t = \vec{\nabla}_t B_z \tag{4}$$

Solving 4 for  $\vec{B}_t$  and plugging into 3, and then the reverse for  $\vec{E}_t$ , give

$$E_t = i \frac{k \vec{\nabla}_t E_z - \omega \hat{z} \times \vec{\nabla}_t B_z}{\omega^2 \mu \epsilon - k^2}$$
 (5)

$$B_t = i \frac{k \vec{\nabla}_t B_z + \omega \mu \epsilon \hat{z} \times \vec{\nabla}_t E_z}{\omega^2 \mu \epsilon - k^2}$$
 (6)

Unless  $k^2 = k_0^2 := \mu \epsilon \omega^2$ ,  $E_z$  and  $B_z$  determine the rest.

We have seen that  $E_z$  and  $B_z$  largely determine the fields. and these satisfy the two-dimensional Helmholtz equation

$$(\nabla_t^2 + \gamma^2) \psi = 0$$
 with  $\gamma^2 = \mu \epsilon \omega^2 - k^2$  (7)

If the walls of the waveguide are very good conductors, we may impose the perfect conductor conditions  $E_{\parallel} \approx 0$  and  $B_{\perp} \approx 0$  on the boundary S of the two-dimensional cross section.  $E_z$  is parallel to the boundary so  $E_z|_S = 0$ . Also the component of  $\vec{E}_t$  parallel to the boundary vanishes at the wall, so  $\vec{E}_t$  is in the  $\pm \hat{n}$  direction. Then from the  $\hat{n}$ component of (2) (normal to the boundary)

$$\frac{\partial \hat{n} \cdot \vec{B}_t}{\partial z} - \hat{n} \cdot \vec{\nabla}_t B_z = i \omega \mu \epsilon \hat{n} \cdot \left( \hat{z} \times \vec{E}_t \right) \Longrightarrow 0 - \frac{\partial B_z}{\partial n} = 0,$$

where  $\partial/\partial n$  is the derivative normal to the surface. So we have Dirichlet conditions on  $E_z$  and Neumann conditions for  $B_{\sim}$ .

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In general, nonzero solutions exist only for discrete values of  $\gamma$ , and those values are generally different for Dirichlet and for Neumann. So we need to consider

- ▶ TEM modes, with  $E_z(x,y) = B_z(x,y) \equiv 0$ . That is, there are no longitudinal fields, both electric (E) and magnetic (M) fields are purely transverse to the direction z of propagation.
- ▶ TE modes,  $E_z(x,y) \equiv 0$ , and the transverse fields are determined by the gradiant of  $B_z = \psi$ , a solution of (7) with Neumann conditions.
- ▶ TM modes,  $B_z(x,y) \equiv 0$ , and the transverse fields are determined by  $E_z = \psi$ , a solution of (7) with zero boundary conditions.

**TEM** modes

With  $E_z(x,y) = B_z(x,y) \equiv 0$ , (5) and (6)  $\Longrightarrow$  everything vanishes or the denominator vanishes,

$$k = \pm k_0$$
 with  $k_0 = \sqrt{\mu \epsilon} \omega$ 

Wave travels  $\parallel z$  with speed  $1/\sqrt{\mu\epsilon}$ , same as for infinite medium. No dispersion.  $\vec{\nabla}_t \cdot \vec{E}_t = 0$  and  $\vec{\nabla}_t \times \vec{E}_t = i\omega B_z = 0$ , so  $\exists \Phi \ni \vec{E}_t = -\vec{\nabla}_t \Phi$ (though  $\Phi$  might not be single valued) and  $\nabla^2 \Phi = 0$ . As  $\vec{E}_{\parallel}|_{S} = 0$ ,  $\Phi = \text{constant on each boundary.}$  If cross section simply connected,  $\Phi = \text{constant}, \vec{E} = 0$ No TEM modes on simply connected cylinder

Yes TEM modes on coaxial cable, or two parallel wires.

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#### TE and TM modes

Equations (5) and (6) simplify for

- TM modes,  $B_z = 0$ ,  $\gamma^2 \vec{E}_t = ik \vec{\nabla}_t E_z$ ,  $\gamma^2 \vec{B}_t = i\mu\epsilon\omega\hat{z} \times \vec{\nabla}_t E_z$ , so  $\vec{H}_t = \epsilon\omega k^{-1}\hat{z} \times \vec{E}_t$ .
- ► TE modes,  $E_z = 0$ ,  $\gamma^2 \vec{B}_t = ik \vec{\nabla}_t B_z$ ,  $\gamma^2 \vec{E}_t = -i\omega \hat{z} \times \vec{\nabla}_t B_z$ , so

$$\vec{E}_t = -\omega \hat{z} \times \vec{B}_t / k \Longrightarrow_{\hat{z} \times} H_t = k \hat{z} \times E_t / \mu \omega.$$

In either case,  $\vec{H}_t = \frac{1}{Z}\hat{z} \times \vec{E}_t$ , with

$$Z = \begin{cases} k/\epsilon \omega = (k/k_0)\sqrt{\mu/\epsilon} & \text{TM} \\ \mu \omega/k = (k_0/k)\sqrt{\mu/\epsilon} & \text{TE} \end{cases}$$



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#### To Summarize

Solutions given by  $\psi(x,y)$ , with  $(\nabla_t^2 + \gamma^2) \psi = 0$ ,  $\gamma^2 = \mu \epsilon \omega^2 - k^2$ , by

 $E_z = \psi e^{ikz - i\omega t}, \quad \vec{E}_t = ik\gamma^{-2} \vec{\nabla}_t \psi e^{ikz - i\omega t}$  $H_z = \psi e^{ikz - i\omega t}, \quad \vec{H}_t = ik\gamma^{-2} \vec{\nabla}_t \psi e^{ikz - i\omega t}$ TE: with  $\hat{n} \cdot \vec{\nabla}_t \psi|_{\Gamma} = 0$ 

By looking at  $0 = \int_A \psi^* (\nabla_t^2 + \gamma^2) \psi$  we can show  $\gamma^2 \ge 0$ . There are solutions for **discrete** values  $\gamma_{\lambda}$ , so only certain wave numbers  $k_{\lambda}$  for a given frequency can propagate:

$$k_{\lambda}^2 = \mu \epsilon \omega^2 - \gamma_{\lambda}^2$$

and only frequencies  $\omega > \omega_{\lambda} := \gamma_{\lambda}/\sqrt{\mu\epsilon}$  can propagate, and  $k_{\lambda} < \sqrt{\mu \epsilon} \omega$ , the infinite medium wavenumber. Phase velocity  $v_p = \omega/k_\lambda$  is greater than in the infinite medium.

### Example: Circular Wave Guide

Jackson does rectangle. You should too. Needed to do homework.

We will consider a circular pipe of (inner) radius r. Of course we should use polar coordinates  $\rho, \phi$ , with

$$\nabla_t^2 = \frac{1}{\rho} \frac{\partial}{\partial \rho} \rho \frac{\partial}{\partial \rho} + \frac{1}{\rho^2} \frac{\partial^2}{\partial \phi^2}, \qquad \text{try} \quad \psi(\rho, \phi) = R(\rho) \Phi(\phi),$$

$$\begin{split} \left(\nabla_t^2 + \gamma^2\right) \psi &= \\ \left(\frac{1}{\rho} \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 R(\rho)\right) \Phi(\phi) + \frac{1}{\rho^2} R(\rho) \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} &= 0. \end{split}$$

Divide by  $R(\rho)\Phi(\phi)$  and multiply by  $\rho^2$ :

$$\begin{split} \frac{1}{R(\rho)} \left( \rho \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 \rho^2 R(\rho) \right) \\ + \frac{1}{\Phi(\phi)} \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} &= 0. \end{split}$$

# Example: Circular Wave Guide

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Divide by  $R(\rho)\Phi(\phi)$  and multiply by  $\rho^2$ :

$$\frac{1}{R(\rho)} \left( \rho \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 \rho^2 R(\rho) \right) = C$$

$$\frac{1}{\Phi(\phi)} \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} = -C.$$

### Solving it

 $\Phi$  first:

$$\frac{\partial^2 \Phi(\phi)}{\partial \phi^2} + C \Phi(\phi) = 0$$

$$\Phi(\phi) = e^{\pm i\sqrt{C}\phi}$$
. Periodicity  $\Longrightarrow \sqrt{C} = m \in \mathbb{Z}$ .

Now  $R(\rho)$ :

$$\left(\rho\frac{\partial}{\partial\rho}\rho\frac{\partial}{\partial\rho}+\gamma^2\rho^2-m^2\right)R(\rho)=0$$

Bessel equation, solutions regular at origin are

$$R(\rho) \propto J_m(\gamma \rho)$$
, so  $\psi(\rho, \phi) = \sum_{m,n} A_{m,n} J_m(\gamma_{mn} \rho) e^{im\phi}$ .

 $\gamma_{mn}$  is determined by boundary conditions...

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Boundary conditions:

For TM,  $\psi(r,\phi) = 0 \Longrightarrow J_m(\gamma r) = 0$ , so  $\gamma_{mn}^{\text{TM}} = x_{mn}/r$ where  $x_{mn}$  is the n'th value of x > 0 for which  $J_m(x) = 0$ , given on page 114.

For TE,  $\hat{n} \cdot \vec{\nabla}_t \psi(r, \phi) = 0 \Longrightarrow \frac{dJ_m}{dr}(\gamma r) = 0$ , so  $\gamma_{mn}^{\text{TM}} = x_{mn}'/r$  where  $x_{mn}'$  is the n'th value of x > 0 for which  $dJ_m(x)/dx = 0$ , given on page 370.

Thus the lowest cutoff frequency is the m=1 TE mode, with  $x'_{11} = 1.841$  while the lowest TM mode or circularly symmetric mode has  $x_{01} = 2.405$ .

For a waveguide 5 cm in diameter, with air or vacuum inside, the cutoff frequencies are  $f = \frac{\omega}{2\pi} = 3.5$  GHz for the lowest TE and 4.6 GHz for the lowest TM modes.

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