Physics 504, Spring 2010 Electricity and Magnetism

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Course Information

- ► Instructor:
 - ▶ Joel Shapiro
 - ► Serin 325
 - ▶ 5-5500 X 3886, shapiro@physics
- ▶ Book: Jackson: Classical Electrodynamics (3rd Ed.)
- Web home page: www.physics.rutgers.edu/grad/504 contains general info, syllabus, lecture and other notes, homework assignments, etc.
- ► Classes: ARC 207, Monday and Thursday, 10:20 (sharp!) 11:40
- ▶ Homework: there will be one or two projects, and homework assignments every week or so. Due dates to be discussed.
- Exams: a midterm and a final.
- ▶ Office Hour: Tuesdays, 3:30–4:30, in Serin 325.

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Last term you covered Jackson, Chapters 1—7 We will cover most of chapters 8—16

Everything comes from Maxwell's Equations and the Lorentz Force. We will discuss:

- ► EM fields confined: waveguides, cavities, optical fibers
- ► Sources of fields: antennas and their radiation, scattering and diffraction
- ▶ Relativity, and relativistic formalism for E&M
- ► Relativistic particles
- ▶ other gauge theories

Maxwell's Equations

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon_0} \rho_{\rm all} \qquad \text{Gauss for E}$$

$$\vec{\nabla} \cdot \vec{B} = 0 \qquad \text{Gauss for B}$$

$$\vec{\nabla} \times \vec{B} - \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} = \mu_0 \vec{J}_{\rm all} \qquad \text{Ampère (+Max)}$$

$$\vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0 \qquad \text{Faraday}$$

plus the Lorentz force:

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

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In the last slide, $\rho_{\rm all}$ and $\vec{J}_{\rm all}$ represent all charges, both "free" and "induced".

Separate "free" from "induced":

- ► For the electric field
 - $ightharpoonup \vec{E}$ called electric field
 - $ightharpoonup \vec{P}$ called *electric polarization* is induced field
 - $ightharpoonup \vec{D}$ called electric displacement is field of "free charges"
 - $\vec{D} = \epsilon_0 \vec{E} + \vec{P}$
- ► For the magnetic field
 - $ightharpoonup \vec{B}$ called magnetic induction (unfortunately)
 - $ightharpoonup \vec{M}$ called magnetization is the induced field
 - $ightharpoonup \vec{H}$ called magnetic field
 - $\vec{H} = \frac{1}{\mu_0} \vec{B} \vec{M}$

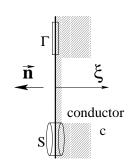
Then the two Maxwell equations with sources, Gauss for \vec{E} and Ampère, get replaced by

$$\vec{\nabla} \cdot \vec{D} = \rho$$

$$\vec{\nabla} \times \vec{H} - \frac{\partial \vec{D}}{\partial t} = \vec{J}$$

Interface between conductor and non-conductor

Conductor c: if perfect, no \vec{E} . Surface charge Σ , eddy currents so no \vec{H} inside conductor. Just outside the conductor: Faraday on loop $\Gamma \longrightarrow E_{\parallel} \approx 0$ Gauss on pillbox $S \longrightarrow B_{\perp} \approx 0$



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$$\vec{\nabla} \times \vec{H}_c = \vec{J} + \frac{\partial \vec{D}}{\partial t} \approx \sigma \vec{E},$$

$$\vec{\nabla} \times \vec{E}_c = -\frac{\partial \vec{B}}{\partial t} = i\omega \mu_c H_c$$

Rapid variation with depth ξ dominates, $\vec{\nabla} = -\hat{n}\frac{\partial}{\partial \xi}$, and

$$\vec{E}_c = \frac{1}{\sigma} \vec{J} = -\frac{1}{\sigma} \hat{n} \times \frac{\partial \vec{H}_c}{\partial \xi}, \qquad \vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi}$$

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$$\vec{E}_c = \frac{1}{\sigma} \vec{J} = -\frac{1}{\sigma} \hat{n} \times \frac{\partial \vec{H}_c}{\partial \xi}, \qquad \vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi}$$

so $\hat{n} \cdot \vec{H}_c = 0$ and

$$\hat{n} \times \vec{H}_c = \frac{i}{\omega \mu_c} \hat{n} \times \left(\hat{n} \times \frac{\partial \vec{E}_c}{\partial \xi} \right)$$

$$= -\frac{i}{\sigma \omega \mu_c} \hat{n} \times \left(\hat{n} \times \left[\hat{n} \times \frac{\partial^2 \vec{H}_c}{\partial \xi^2} \right] \right)$$

$$= \frac{i}{\sigma \omega \mu_c} \frac{\partial^2}{\partial \xi^2} \left(\hat{n} \times \vec{H}_c \right).$$

Simple DEQ, exponential solution, with $\delta = \sqrt{\frac{2}{\mu_c \omega \sigma}}$,

$$\vec{H}_c = \vec{H}_{\parallel} e^{-\xi/\delta} e^{i\xi/\delta},$$

 H_{\parallel} is tangential field outside surface of conductor.

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From $\vec{H}_c = \vec{H}_{\parallel} e^{-\xi/\delta} e^{i\xi/\delta}$

$$\vec{E}_c = -\frac{1}{\sigma}\hat{n} \times \frac{\partial \vec{H}_c}{\partial \xi} = \sqrt{\frac{\mu_c \omega}{2\sigma}} (1 - i)\hat{n} \times \vec{H}_{\parallel} e^{-\xi/\delta} e^{i\xi/\delta},$$

which means, by continuity, that just outside the conductor

$$\vec{E}_{\parallel} = \sqrt{\frac{\mu_c \omega}{2\sigma}} (1 - i) \hat{n} \times \vec{H}_{\parallel}.$$

$$\frac{dP_{\text{loss}}}{dA} = -\hat{n} \cdot \langle \vec{S} \rangle
= -\frac{1}{2} \sqrt{\frac{\mu_c \omega}{2\sigma}} \hat{n} \cdot \text{Re} \left[(1 - i)(\hat{n} \times \vec{H}_{\parallel}) \times \vec{H}_{\parallel}^* \right]
= \frac{\mu_c \omega \delta}{4} |\vec{H}_{\parallel}|^2 = \frac{1}{2\sigma \delta} |\vec{H}_{\parallel}|^2$$

Method 2, Ohmic heating, power lost per unit volume $\frac{1}{2}\vec{J}\cdot\vec{E}^* = |\vec{J}|^2/2\sigma$, $|\vec{J}| = \sigma\vec{E}_c = \frac{\sqrt{2}}{\delta}|\vec{H}_{\parallel}|e^{-\xi/\delta}$, the power loss per unit area is

$$\frac{dP_{\text{loss}}}{dA} = \frac{1}{\delta^2 \sigma} |\vec{H}_{\parallel}|^2 \int_0^{\infty} d\xi \, e^{-2\xi/\delta} = \frac{1}{2\delta \sigma} |\vec{H}_{\parallel}|^2.$$

Agrees with method 1.

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In terms of surface current

$$\begin{split} \vec{K}_{\text{eff}} &= \int_0^\infty d\xi \, \vec{J}(\xi) = \frac{1}{\delta} \hat{n} \times \vec{H}_{\parallel} \int_0^\infty d\xi \, (1-i) e^{-\xi(1-i)/\delta} \\ &= \hat{n} \times \vec{H}_{\parallel}. \end{split}$$

Thus

$$\frac{dP_{\rm loss}}{dA} = \frac{1}{2\sigma\delta} |\vec{K}_{\rm eff}|^2.$$

 $\frac{1}{\sigma\delta}$ is surface resistance (per unit area) and $\frac{\vec{E}_{\parallel}}{\vec{K}_{\text{eff}}} = \frac{1-i\delta}{\sigma\delta}$ is the surface impediance Z.

For electromagnetic fields with a fixed geometry of linear materials, fourier transform decouples, and we can work with frequency modes,

$$\begin{array}{lcl} \vec{E}(\vec{x},t) & = & \vec{E}(x,y,z) \ e^{-i\omega t} \\ \vec{B}(\vec{x},t) & = & \vec{B}(x,y,z) \ e^{-i\omega t} \\ \end{array}$$

Actually the fields are the real parts of these complex expressions.

If $\rho = 0$, $\vec{J} = 0$, Maxwell gives

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = i\omega \vec{B}, \qquad \vec{\nabla} \cdot \vec{E} = 0, \qquad \vec{\nabla} \cdot \vec{B} = 0,$$

$$\vec{\nabla} \times \vec{B} = \mu \vec{\nabla} \times \vec{H} = \mu \frac{\partial \vec{D}}{\partial t} = \mu \epsilon \frac{\partial \vec{E}}{\partial t} = -i\omega \mu \epsilon \vec{E}.$$

Then

$$\nabla^2 \vec{E} = -\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) + \vec{\nabla} \left(\vec{\nabla} \cdot \vec{E} \right) = -\vec{\nabla} \times (i\omega \vec{B}) = -\omega^2 \mu \epsilon \vec{E}.$$

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$$(\nabla^2 + \omega^2 \mu \epsilon) \vec{E} = 0, \qquad (\nabla^2 + \omega^2 \mu \epsilon) \vec{B} = 0.$$

Consider a waveguide, a cylinder of arbitrary cross section but uniform in z. Fourier transform in z

$$\vec{E}(x, y, z, t) = \vec{E}(x, y)e^{ikz-i\omega t}$$

 $\vec{B}(x, y, z, t) = \vec{B}(x, y)e^{ikz-i\omega t}$

k can take either sign (and a standing wave is a superposition of $k=\pm |k|$). The Helmholtz equations give

$$\left[\nabla_t^2 + (\mu\epsilon\omega^2 - k^2)\right] \begin{pmatrix} \vec{E}(x,y) \\ \vec{B}(x,y) \end{pmatrix} = 0, \quad \nabla_t^2 := \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}.$$

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Decompose longitudinal and transverse

Let

$$\vec{E} = E_z \hat{z} + \vec{E}_t \\ \vec{B} = B_z \hat{z} + \vec{B}_t$$
 with $\vec{E}_t \perp \hat{z} \\ \vec{B}_t \perp \hat{z}$

$$(\vec{\nabla} \times \vec{E})_z = (\vec{\nabla}_t \times \vec{E}_t)_z = i\omega B_z,$$

$$(\vec{\nabla} \times \vec{E})_{\perp} = \hat{z} \times \frac{\partial \vec{E}_t}{\partial z} - \hat{z} \times \nabla_t E_z = i\omega \vec{B}_t.$$

For any vector \vec{V} , $\hat{z} \times (\hat{z} \times \vec{V}) = -\vec{V} + \hat{z}(\hat{z} \cdot V)$, so for a transverse vector $\hat{z} \times (\hat{z} \times \vec{V}_t) = -\vec{V}_t$. Taking $\hat{z} \times$ last equation,

$$\frac{\partial E_t}{\partial z} - \vec{\nabla}_t E_z = -i\omega \hat{z} \times \vec{B}_t. \tag{1}$$

Similarly decomposition of $\vec{\nabla} \times \vec{B} = -i\omega\mu\epsilon\vec{E}$ gives

$$\left(\vec{\nabla}_t \times \vec{B}_t \right)_z = -i\omega\mu\epsilon E_z$$

$$\frac{\partial \vec{B}_t}{\partial z} - \vec{\nabla}_t B_z = i\omega\mu\epsilon \hat{z} \times \vec{E}_t.$$

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Divergencelessness:

$$\vec{\nabla}_t \cdot \vec{E}_t + \frac{\partial E_z}{\partial z} = 0, \qquad \vec{\nabla}_t \cdot \vec{B}_t + \frac{\partial B_z}{\partial z} = 0.$$

Equations (1) and (2), with the fourier transform in z, give

$$ik\vec{B}_t - i\omega\mu\epsilon\hat{z} \times \vec{E}_t = \vec{\nabla}_t B_z$$
 (4)
For \vec{B}_t and plugging into 3, and then the reverse

Solving 4 for B_t and plugging into 3, and then the reverse for \vec{E}_t , give

 $ik\vec{E}_t + i\omega\hat{z} \times \vec{B}_t = \vec{\nabla}_t E_z$

$$E_t = i \frac{k \vec{\nabla}_t E_z - \omega \hat{z} \times \vec{\nabla}_t B_z}{\omega^2 \mu \epsilon - k^2}$$
 (5)

$$\omega^{2}\mu\epsilon - k^{2}$$

$$k\vec{\nabla}_{t}B_{z} + \omega\mu\epsilon\hat{z} \times \vec{\nabla}_{t}E_{z}$$
(6)

$$B_t = i \frac{k \vec{\nabla}_t B_z + \omega \mu \epsilon \hat{z} \times \vec{\nabla}_t E_z}{\omega^2 \mu \epsilon - k^2}$$
 (6)

Unless $k^2 = k_0^2 := \mu \epsilon \omega^2$, E_z and B_z determine the rest.

(3)

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$$(\nabla_t^2 + \gamma^2) \psi = 0$$
 with $\gamma^2 = \mu \epsilon \omega^2 - k^2$ (7)

If the walls of the waveguide are very good conductors, we may impose the perfect conductor conditions $E_{\parallel} \approx 0$ and $B_{\perp} \approx 0$ on the boundary S of the two-dimensional cross section. E_z is parallel to the boundary so $E_z|_S = 0$. Also the component of \vec{E}_t parallel to the boundary vanishes at the wall, so \vec{E}_t is in the $\pm \hat{n}$ direction. Then from the \hat{n} component of (2) (normal to the boundary)

$$\frac{\partial \hat{n} \cdot \vec{B}_t}{\partial z} - \hat{n} \cdot \vec{\nabla}_t B_z = i\omega \mu \epsilon \hat{n} \cdot \left(\hat{z} \times \vec{E}_t\right) \Longrightarrow 0 - \frac{\partial B_z}{\partial n} = 0,$$

where $\partial/\partial n$ is the derivative normal to the surface. So we have Dirichlet conditions on E_z and Neumann conditions for B_z .

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- ▶ TEM modes, with $E_z(x,y) = B_z(x,y) \equiv 0$. That is, there are no longitudinal fields, both electric (E) and magnetic (M) fields are purely transverse to the direction z of propagation.
- ▶ TE modes, $E_z(x,y) \equiv 0$, and the transverse fields are determined by the gradiant of $B_z = \psi$, a solution of (7) with Neumann conditions.
- ► TM modes, $B_z(x,y) \equiv 0$, and the transverse fields are determined by $E_z = \psi$, a solution of (7) with zero boundary conditions.

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$$k = \pm k_0$$
 with $k_0 = \sqrt{\mu \epsilon} \omega$

Wave travels $\parallel z$ with speed $1/\sqrt{\mu\epsilon}$, same as for infinite medium. No dispersion.

 $\vec{\nabla}_t \cdot \vec{E}_t = 0$ and $\vec{\nabla}_t \times \vec{E}_t = i\omega B_z = 0$, so $\exists \Phi \ni \vec{E}_t = -\vec{\nabla}_t \Phi$ (though Φ might not be single valued) and $\nabla^2 \Phi = 0$. As $\vec{E}_{\parallel} \Big|_{\alpha} = 0$, $\Phi = \text{constant on each boundary.}$ If cross

As $E_{\parallel}|_{S} = 0$, $\Phi = \text{constant}$ on each boundary. If cross section simply connected, $\Phi = \text{constant}$, $\vec{E} = 0$ No TEM modes on simply connected cylinder Yes TEM modes on coaxial cable, or two parallel wires. Physics 504, Spring 2010 Electricity and Magnetism

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Equations (5) and (6) simplify for

- ► TM modes, $B_z = 0$, $\gamma^2 \vec{E}_t = ik \vec{\nabla}_t E_z$, $\gamma^2 \vec{B}_t = i\mu\epsilon\omega\hat{z} \times \vec{\nabla}_t E_z$, so $\vec{H}_t = \epsilon\omega k^{-1}\hat{z} \times \vec{E}_t$.
- ► TE modes, $E_z = 0$, $\gamma^2 \vec{B}_t = ik \vec{\nabla}_t B_z$, $\gamma^2 \vec{E}_t = -i\omega \hat{z} \times \vec{\nabla}_t B_z$, so

$$\vec{E}_t = -\omega \hat{z} \times \vec{B}_t / k \Longrightarrow_{\hat{z} \times} H_t = k \hat{z} \times E_t / \mu \omega.$$

In either case, $\vec{H}_t = \frac{1}{Z}\hat{z} \times \vec{E}_t$, with

$$Z = \begin{cases} k/\epsilon\omega = (k/k_0)\sqrt{\mu/\epsilon} & \text{TM} \\ \mu\omega/k = (k_0/k)\sqrt{\mu/\epsilon} & \text{TE} \end{cases}$$

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To Summarize

Solutions given by $\psi(x, y)$, with $(\nabla_t^2 + \gamma^2) \psi = 0$, $\gamma^2 = \mu \epsilon \omega^2 - k^2$, by

TM:
$$E_z = \psi e^{ikz - i\omega t}, \quad \vec{E}_t = ik\gamma^{-2}\vec{\nabla}_t\psi e^{ikz - i\omega t}$$

with $\psi|_{\Gamma} = 0$
TE: $H_z = \psi e^{ikz - i\omega t}, \quad \vec{H}_t = ik\gamma^{-2}\vec{\nabla}_t\psi e^{ikz - i\omega t}$
with $\hat{n} \cdot \vec{\nabla}_t\psi|_{\Gamma} = 0$

By looking at $0 = \int_A \psi^* \left(\nabla_t^2 + \gamma^2 \right) \psi$ we can show $\gamma^2 \ge 0$. There are solutions for **discrete** values γ_{λ} , so only certain wave numbers k_{λ} for a given frequency can propagate:

$$k_{\lambda}^2 = \mu \epsilon \omega^2 - \gamma_{\lambda}^2,$$

and only frequencies $\omega > \omega_{\lambda} := \gamma_{\lambda}/\sqrt{\mu\epsilon}$ can propagate, and $k_{\lambda} < \sqrt{\mu\epsilon} \omega$, the infinite medium wavenumber. Phase velocity $v_p = \omega/k_{\lambda}$ is greater than in the infinite medium.

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Example: Circular Wave Guide

Jackson does rectangle. You should too. Needed to do homework.

We will consider a circular pipe of (inner) radius r. Of course we should use polar coordinates ρ, ϕ , with

$$\nabla_t^2 = \frac{1}{\rho} \frac{\partial}{\partial \rho} \rho \frac{\partial}{\partial \rho} + \frac{1}{\rho^2} \frac{\partial^2}{\partial \phi^2}, \quad \text{try} \quad \psi(\rho, \phi) = R(\rho) \Phi(\phi),$$
$$\left(\nabla_t^2 + \gamma^2\right) \psi = \left(\frac{1}{\rho} \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 R(\rho)\right) \Phi(\phi) + \frac{1}{\rho^2} R(\rho) \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} = 0.$$

Divide by $R(\rho)\Phi(\phi)$ and multiply by ρ^2 :

$$\begin{split} \frac{1}{R(\rho)} \left(\rho \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 \rho^2 R(\rho) \right) \\ + \frac{1}{\Phi(\phi)} \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} &= 0. \end{split}$$

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$$(\nabla_t^2 + \gamma^2) \psi =$$

$$\left(\frac{1}{\rho}\frac{\partial}{\partial\rho}\rho\frac{\partial R}{\partial\rho} + \gamma^2 R(\rho)\right)\Phi(\phi) + \frac{1}{\rho^2}R(\rho)\frac{\partial^2 \Phi(\phi)}{\partial\phi^2} = 0.$$

Divide by $R(\rho)\Phi(\phi)$ and multiply by ρ^2 :

$$\frac{1}{R(\rho)} \left(\rho \frac{\partial}{\partial \rho} \rho \frac{\partial R}{\partial \rho} + \gamma^2 \rho^2 R(\rho) \right) = C$$

$$\frac{1}{\Phi(\phi)} \frac{\partial^2 \Phi(\phi)}{\partial \phi^2} = -C.$$

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 Φ first:

$$\frac{\partial^2 \Phi(\phi)}{\partial \phi^2} + C\Phi(\phi) = 0$$

$$\Phi(\phi) = e^{\pm i\sqrt{C}\phi}$$
. Periodicity $\Longrightarrow \sqrt{C} = m \in \mathbb{Z}$.

Now $R(\rho)$:

$$\left(\rho\frac{\partial}{\partial\rho}\rho\frac{\partial}{\partial\rho}+\gamma^2\rho^2-m^2\right)R(\rho)=0$$

Bessel equation, solutions regular at origin are

$$R(\rho) \propto J_m(\gamma \rho)$$
, so $\psi(\rho, \phi) = \sum_{m,n} A_{m,n} J_m(\gamma_{mn} \rho) e^{im\phi}$.

 γ_{mn} is determined by boundary conditions...

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For TE, $\hat{n} \cdot \vec{\nabla}_t \psi(r, \phi) = 0 \Longrightarrow \frac{dJ_m}{dr}(\gamma r) = 0$, so $\gamma_{mn}^{\text{TM}} = x'_{mn}/r$ where x'_{mn} is the *n*'th value of x > 0 for which $dJ_m(x)/dx = 0$, given on page 370.

Thus the lowest cutoff frequency is the m = 1 TE mode, with $x'_{11} = 1.841$ while the lowest TM mode or circularly symmetric mode has $x_{01} = 2.405$.

For a waveguide 5 cm in diameter, with air or vacuum inside, the cutoff frequencies are $f = \frac{\omega}{2\pi} = 3.5$ GHz for the lowest TE and 4.6 GHz for the lowest TM modes.

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