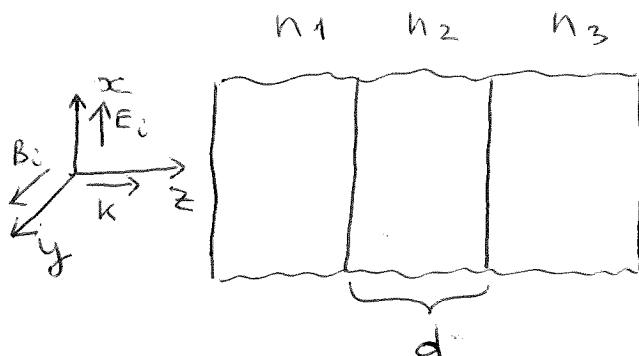


HW #3 solutions

7.2



Non-magnetic media

(a) Choose a coordinate system s.t.

$$\begin{cases} \vec{E}_i = E_i e^{i(k_1 z - \omega t)} \hat{x}, & \text{incident wave} \\ \vec{B}_i = \frac{k_1 E_i}{\omega} e^{i(k_1 z - \omega t)} \hat{y} \end{cases}$$

$\frac{E_i}{v_1}$, v_1 - phase velocity in medium n_1
 k_1 - wave number in medium n_1

Likewise,

$$\begin{cases} \vec{E}_r = E_r e^{i(-k_1 z - \omega t)} \hat{x}, & \text{reflected wave} \\ \vec{B}_r = -\frac{E_r}{v_1} e^{i(-k_1 z - \omega t)} \hat{y} \end{cases}$$

Note that multiple reflections from both boundaries are included into E_r .

In medium n_2 , there are 2 waves as well:

$$\begin{cases} \vec{E}_+ = E_+ e^{i(k_2 z - \omega t)} \hat{x}, & \text{propagates to the right} \\ \vec{B}_+ = \frac{E_+}{v_2} e^{i(k_2 z - \omega t)} \hat{y} \\ \vec{E}_- = E_- e^{i(-k_2 z - \omega t)} \hat{x}, & \text{propagates to the left} \\ \vec{B}_- = -\frac{E_-}{v_2} e^{i(-k_2 z - \omega t)} \hat{y} \end{cases}$$

Again, E_+ , E_- include multiple reflection events.

Finally, in medium n_3 we have:

$$\begin{cases} \vec{E}_t = E_t e^{i(k_3 z - \omega t)} \hat{x}, \\ \vec{B}_t = \frac{E_t}{v_3} e^{i(k_3 z - \omega t)} \hat{y}. \end{cases}$$

There is no reflected wave.

Now, use BCs:
$$\begin{cases} \vec{E}''(0^-) = \vec{E}''(0^+), \\ \vec{B}''(0^-) = \vec{B}''(0^+). \end{cases}$$

Here, 0 & d are z -coordinates of the two interfaces

$$\begin{cases} \vec{E}''(d^-) = \vec{E}''(d^+), \\ \vec{B}''(d^-) = \vec{B}''(d^+). \end{cases}$$

$x=0$:
$$\begin{cases} E_i + E_r = E_t + E_-, \\ \frac{E_i - E_r}{v_1} = \frac{E_t - E_-}{v_2}. \end{cases}$$

$x=d$:
$$\begin{cases} E_+ e^{ik_2 d} + E_- e^{-ik_2 d} = E_t e^{ik_3 d}, \\ \frac{E_+ e^{ik_2 d} - E_- e^{-ik_2 d}}{v_2} = \frac{E_t e^{ik_3 d}}{v_3}. \end{cases}$$

The rest is algebra ...

Define
$$\begin{cases} a_1 = \frac{v_1}{v_2} = \frac{c/n_1}{c/n_2} = \frac{n_2}{n_1}, \\ a_2 = \frac{v_2}{v_3} = \frac{n_3}{n_2}. \end{cases}$$

Then
$$\begin{cases} E_i + E_r = E_t + E_-, & (1) \\ E_i - E_r = a_1 (E_t - E_-) & (2) \end{cases}$$

$$E_+ e^{ik_2 d} + E_- e^{-ik_2 d} = E_t e^{ik_3 d}, \quad (3)$$

$$E_+ e^{ik_2 d} - E_- e^{-ik_2 d} = a_2 E_t e^{ik_3 d} \quad (4)$$

Eqs. (3) & (4) give:

$$\begin{cases} E_+ e^{ik_2 d} = \frac{1+a_2}{2} E_t e^{ik_3 d} \\ E_- e^{-ik_2 d} = \frac{1-a_2}{2} E_t e^{ik_3 d} \end{cases}$$

Then Eqs. (1) & (2) give:

$$\begin{aligned} 2E_i &= (1+a_1)E_+ + (1-a_1)E_- = \\ &= \frac{(1+a_1)(1+a_2)}{2} E_t e^{i(k_3-k_2)d} + \\ &+ \frac{(1-a_1)(1-a_2)}{2} E_t e^{i(k_3+k_2)d} \end{aligned}$$

Then

$$\begin{aligned} \frac{E_i}{E_t} &= \frac{1}{2} e^{ik_3 d} \left\{ \frac{(1+a_1)(1+a_2)}{2} e^{-ik_2 d} + \right. \\ &\quad \left. + \frac{(1-a_1)(1-a_2)}{2} e^{ik_2 d} \right\} = \\ &= \frac{e^{ik_3 d}}{2} \left\{ (1+a_1 a_2) \cos(k_2 d) - \right. \\ &\quad \left. - i(a_1 + a_2) \sin(k_2 d) \right\} \end{aligned}$$

Then

$$4 \left| \frac{E_i}{E_t} \right|^2 = (1+a_1 a_2)^2 \cos^2(k_2 d) + (a_1 + a_2)^2 \sin^2(k_2 d) =$$

$$= (1+a_1 a_2)^2 - (1-a_1^2)(1-a_2^2) \sin^2(k_2 d) \quad (*)$$

Finally, the transmission coeff.

$$T = \frac{I_t}{I_i} = \frac{\epsilon_3 v_3 |E_t|^2}{\epsilon_1 v_1 |E_i|^2} = \frac{\overbrace{n_3}^{a_1 a_2}}{n_1} \frac{|E_t|^2}{|E_i|^2} =$$

$$\overbrace{\frac{4 a_1 a_2}{(1+a_1 a_2)^2 - (1-a_1^2)(1-a_2^2) \sin^2(k_2 d)}}^{(*)}$$

In other words,

$$T = \frac{4n_1 n_2^2 n_3}{n_2^2 (n_1 + n_3)^2 + (n_2^2 - n_3^2)(n_2^2 - n_1^2) \sin^2(n_2 \frac{\omega}{c} d)}$$

The reflection coeff. $R = 1 - T$.

These (T & R) can be plotted as a f'n of ω .

What happens if $d=0$?

$$\left\{ \begin{aligned} T &= \frac{4n_1 n_3}{(n_1 + n_3)^2}, \\ R &= 1 - T = \frac{n_1^2 + 2n_1 n_3 + n_3^2 - 4n_1 n_3}{(n_1 + n_3)^2} = \frac{(n_1 - n_3)^2}{(n_1 + n_3)^2}. \end{aligned} \right.$$

→ Single interface limit (no n_2 dependence as expected)

(b) $n_3=1$; find n_2 & d so there is no reflection @ ω_0 .

If $n_3=1$,

$$R = \frac{n_2^2 (n_1 - 1)^2 + (n_2^2 - 1)(n_2^2 - n_1^2) \sin^2(n_2 \frac{\omega_0}{c} d)}{n_2^2 (n_1 + 1)^2 + (n_2^2 - 1)(n_2^2 - n_1^2) \sin^2(n_2 \frac{\omega_0}{c} d)}$$

We require

$$\underbrace{n_2^2 (n_1 - 1)^2}_{>0 (n_1 > 1)} + \underbrace{(n_2^2 - 1)}_{>0 (n_2 > 1)} \underbrace{(n_2^2 - n_1^2)}_{\text{may be } < 0 \text{ if } n_2 < n_1} \underbrace{\sin^2(n_2 \frac{\omega_0}{c} d)}_{>0} = 0$$

This is one eq'n for 2 unknowns: n_2 & $d \Rightarrow$

\Rightarrow multiple solutions

One possibility:

$$\begin{cases} \sin^2(\dots) = 1, & \Rightarrow d = \frac{c}{n_2 \omega_0} \overbrace{\pi \left(i + \frac{1}{2} \right)}^{\sin = \pm 1} \\ n_2^2 (n_1 - 1)^2 + (n_2^2 - 1)(n_2^2 - n_1^2) = 0 \end{cases}$$

\uparrow integer

$$\Downarrow n_2 = \sqrt{n_1}$$

$$n_1 (n_1 - 1)^2 + (n_1 - 1)(n_1 - n_1^2) =$$

$$= n_1 (n_1 - 1)^2 - n_1 (n_1 - 1)^2 = 0$$

So, $\begin{cases} n_2 = \sqrt{n_1}, \\ d = \frac{c}{\sqrt{n_1} \omega_0} \pi \left(i + \frac{1}{2} \right) \end{cases}$ should work

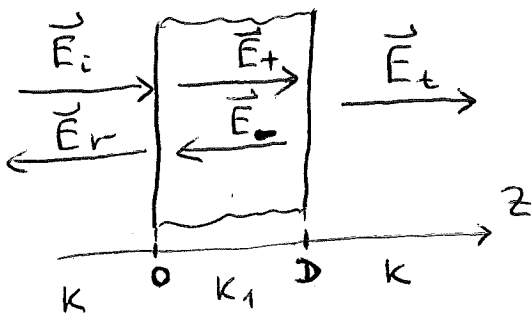
7.5

$\vec{E} = \vec{E}_i e^{i(\vec{k}\vec{x} - \omega t)}$; normal incidence
Conductor with $\sigma \gg \omega\epsilon_0$,
thickness D .

a) Recall that

$$\epsilon = \epsilon_0 + i \frac{\sigma}{\omega}$$

Use BCs as in 7.2:



$$\underline{z=0}: \begin{cases} E_i + E_r = E_+ + E_- \\ E_i - E_r = n(E_+ - E_-) \end{cases} \quad (*)$$

$$n = \sqrt{\frac{\epsilon}{\epsilon_0}} = \sqrt{1 + i \frac{\sigma}{\omega\epsilon_0}}$$

$$\underline{z=D}: \begin{cases} E_+ e^{i\gamma D} + E_- e^{-i\gamma D} = E_t e^{ikD} \\ n(E_+ e^{i\gamma D} - E_- e^{-i\gamma D}) = E_t e^{ikD} \end{cases} \quad (**)$$

Note that

$$\gamma = k_1 D = \frac{\omega n}{c} D = \frac{\omega}{c} D \sqrt{1 + i \frac{\sigma}{\omega\epsilon_0}}$$

$$\text{If } \frac{\epsilon}{\omega \epsilon_0} \gg 1, \quad n \approx \sqrt{i \frac{\epsilon}{\omega \epsilon_0}} = \frac{2}{\gamma},$$

$$\text{where } \gamma = \sqrt{\frac{2 \epsilon_0 \omega}{\epsilon}} (1-i)$$

Moreover,

$$\gamma = \frac{\omega n}{c} D \approx \frac{\omega}{c} D \frac{2}{\gamma} = i \lambda \quad \underbrace{(1-i) \frac{D}{\delta}}_{\delta = \sqrt{\frac{2}{\omega \mu \epsilon}} \text{ is the penetr'n depth}}$$

$$\text{Thus } |n| \gg 1 \Rightarrow |\gamma| \ll 1.$$

We can use eq's (*) & (**) to

express $\frac{E_r}{E_i}$ & $\frac{E_t}{E_i}$ in terms of γ & λ :
(best done in Mathematica)

$$\left\{ \begin{array}{l} \frac{E_r}{E_i} = \frac{e^{-2\lambda} - 1}{(1 - e^{-2\lambda}) + \gamma(1 + e^{-2\lambda})}, \\ \frac{E_t}{E_i} = e^{-i k D} \frac{2\gamma e^{-\lambda}}{(1 - e^{-2\lambda}) + \gamma(1 + e^{-2\lambda})} \end{array} \right.$$

Note that all $O(\gamma^2)$ terms have been dropped. Also, there is an overall

↑
(but could've been kept in principle)

phase factor $\sim e^{-i k D}$ which appears to have been dropped in Jackson (it does not affect $|\frac{E_t}{E_i}|^2$ anyway)

b) $D \rightarrow 0$ implies $\lambda \rightarrow 0$.

$$\text{Then } \begin{cases} \frac{E_r}{E_i} \rightarrow 0, \\ \frac{E_t}{E_i} \rightarrow 1, \text{ as expected.} \end{cases}$$

$D \rightarrow \infty \Rightarrow \lambda \rightarrow \infty$:

$$\begin{cases} \frac{E_t}{E_i} \rightarrow 0, \\ \frac{E_r}{E_i} \rightarrow -\frac{1}{1+\gamma}. \end{cases}$$

Note that some power is dissipated in the conductor. If $\sigma \rightarrow \infty \Rightarrow \Rightarrow \gamma \rightarrow 0 \Rightarrow \frac{E_r}{E_i} \rightarrow -1$, everything gets reflected in the perfect conductor.

c) "Very small thickness": this is about simplifying the denominator in $\frac{E_t}{E_i}$. We cannot say that

$$\begin{aligned} \text{denominator } (1 - e^{-2\lambda}) + \gamma(1 + e^{-2\lambda}) &\approx \\ &\approx 1 - e^{-2\lambda} \quad \text{IF} \end{aligned}$$

$$|1 - e^{-2\lambda}| \approx |\gamma(1 + e^{-2\lambda})|.$$

D is small $\Rightarrow \lambda$ is small, s.t.

$$|\lambda| \approx |\gamma|, \text{ or } \frac{D}{\delta} \approx \frac{\omega \delta}{c},$$

$$D \approx \frac{\omega \delta^2}{c}.$$

So, $D \leq \frac{\omega \delta^2}{c}$ is the small thickness limit.

$$\text{If } D > \frac{\omega \delta^2}{c}, \quad \frac{E_t}{E_i} \approx e^{-ikD} \frac{2\gamma e^{-\lambda}}{1 - e^{-2\lambda}}.$$

$$\text{Then } T = \left| \frac{E_t}{E_i} \right|^2 = \frac{4\gamma\gamma^* e^{-\lambda + \lambda^*}}{(1 - e^{-2\lambda})(1 - e^{-2\lambda^*})}.$$

$$\text{Note that } |\gamma|^2 = 2 \frac{2\epsilon_0 \omega}{\delta} = 2 (\text{Re}(\gamma))^2.$$

$$\text{Also, } e^{-\lambda} = e^{-D/\delta} e^{iD/\delta}.$$

$$\text{Then } T = \frac{8 (\text{Re}(\gamma))^2 e^{-2D/\delta}}{1 + e^{-4D/\delta} - 2 e^{-2D/\delta} \cos(2D/\delta)}.$$

7.4 σ, ϵ free space / medium interface

(a) Normal incidence:

$$\frac{\vec{E}_0''}{\vec{E}_0} = \frac{1-n}{1+n}$$

reflected
incident

Recall that $n = c/v = c\sqrt{\mu\epsilon}$.

We have argued that for a conductor, we can neglect $\epsilon(\omega)$, yielding
 $\epsilon = \frac{i\sigma}{\omega}$ (true for low ω , or large σ)

Then
$$n = c\sqrt{i\frac{\mu\sigma}{\omega}} = (1+i) \frac{c}{\omega} \sqrt{\frac{\mu\sigma\omega}{2}} =$$

$\sqrt{\frac{1+i}{2}}$ $\sqrt{\frac{\mu\sigma\omega}{2}}$
 k^{-1} $\omega^{\frac{1}{2}}$

$$= (1+i) \frac{1}{k\delta}$$
, where $[\delta] = L$,
 δ - skin depth.

Finally,
$$\frac{E_0''}{E_0} = \frac{1 - (1+i) \frac{1}{k\delta}}{1 + (1+i) \frac{1}{k\delta}} \equiv r e^{i\phi}$$

 complex

after some algebra,

$$\begin{cases} r = \frac{\sqrt{\omega^4 \delta^4 + 4c^4}}{2c^2 + 2c\omega\delta + \omega^2 \delta^2}, \\ \tan \phi = -\frac{2c\omega\delta}{\omega^2 \delta^2 - 2c^2}. \end{cases}$$

(b)

Note that $\delta = \sqrt{\frac{2}{\mu\sigma\omega}} \rightarrow 0$ as $\sigma \rightarrow +\infty$ (good conductor)

Then $r \rightarrow 1$, $\tan \phi \rightarrow 0^+ \Rightarrow \phi \rightarrow \pi$
 \uparrow phase change due to $n > 1$

The reflected wave must have a phase change since $n > 1$.

~~(11)~~ For a good conductor,

$$R = r^2 = \frac{\omega^4 \delta^4 + 4c^4}{(2c^2 + 2(\omega\delta + \omega^2\delta^2))^2} \approx \begin{matrix} \uparrow \\ \text{expand to } O(\delta) \end{matrix}$$
$$\approx 1 - 2 \frac{\omega}{c} \delta$$

For a poor conductor,

$$\delta \rightarrow 0 \quad \& \quad \delta \rightarrow +\infty$$

In this limit, $\epsilon_b(\omega)$ cannot be neglected & $\epsilon = i\frac{\sigma}{\omega}$ breaks down.
The medium behaves as a regular insulator.