

## HW #1 solutions

### 12.2 A Hall Thruster

- (a) We get uniform electron drift in the  $z$ -direction if the electric force density  $-en_e\mathbf{E}$  exactly cancels the Lorentz magnetic force density  $-en_e\mathbf{v}\times\mathbf{B}$ . Imposing this condition,  $\mathbf{E} = -\mathbf{v}\times\mathbf{B}$ , implies that

$$\mathbf{E}\times\mathbf{B} = \mathbf{B}\times(\mathbf{v}\times\mathbf{B}) = \mathbf{v}B^2 - \mathbf{B}(\mathbf{B}\cdot\mathbf{v}).$$

This, in turn, implies the suggested result,

$$\mathbf{v} = \frac{\mathbf{E}\times\mathbf{B}}{B^2}.$$

- (b) Using the equality of the forces in part (a) and  $n_i = n_e$ , the electric force on the ions is

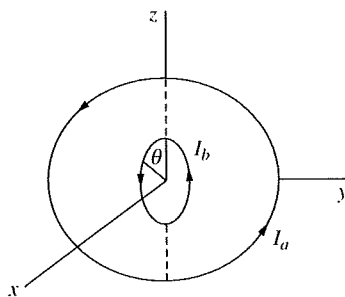
$$\mathbf{F}_i = en_i\mathbf{E} = en_e\mathbf{E} = -en_e\mathbf{v}\times\mathbf{B} = \mathbf{j}_{\text{Hall}}\times\mathbf{B}.$$

By Newton's third law, the reaction thrust on the shells is  $\mathbf{T} = -\mathbf{F}_i = \mathbf{B}\times\mathbf{j}_{\text{Hall}}$  if the ions are ejected from  $V$  before the magnetic Lorentz force on the ions begins to act. This will be the case because a xenon ion is much more massive than an electron.



### 12.6 The Torque between Nested Current Rings

We locate the ring  $I_a$  in the  $x$ - $y$  plane and the ring  $I_b$  in the  $x$ - $z$  plane as shown below. The magnetic field on the axis of  $I_a$  points in the  $z$ -direction. The magnetic field of  $I_b$  points in the  $y$ -direction.



The vector torque which acts on  $I_b$  is

$$\mathbf{N} = I_b \oint \mathbf{r} \times (d\boldsymbol{\ell} \times \mathbf{B}),$$

where  $\mathbf{r} = b \cos \theta \hat{\mathbf{z}} + b \sin \theta \hat{\boldsymbol{\theta}}$ ,  $d\boldsymbol{\ell} = b d\theta \hat{\boldsymbol{\theta}} = b d\theta (\cos \theta \hat{\mathbf{x}} - \sin \theta \hat{\mathbf{z}})$ , and  $\mathbf{B} = B_\rho \hat{\boldsymbol{\rho}} + B_z \hat{\mathbf{z}}$  is the magnetic field due to  $I_a$  in cylindrical coordinates. Since parallel currents attract and anti-parallel currents repel, the only component of the torque which survives is  $N_x$ . Focusing on this component, substituting  $\mathbf{r}$ ,  $d\boldsymbol{\ell}$ , and  $\mathbf{B}$  into the torque formula gives

$$N_x = I_b b^2 \int_0^{2\pi} d\theta \cos \theta (B_z \cos \theta + B_\rho \sin \theta).$$

Our task now is to write the components of  $\mathbf{B}(\rho, z)$  near the origin, where  $\rho = b \sin \theta$  and  $z = b \cos \theta$ . In the text, we used the technique of “going off the axis” to find the exact magnetic scalar potential of a current loop. In polar coordinates, the first two terms of this expansion for  $r < a$  were

$$\psi(r, \theta) = -\frac{1}{2} \mu_0 I_a \left[ \frac{r}{a} P_0(0) P_1(\cos \theta) + \left(\frac{r}{a}\right)^3 P_2(0) P_3(\cos \theta) \right].$$

Using  $P_0 = 1$ ,  $P_1 = \cos \theta$ ,  $P_2 = (1/2)(3 \cos^2 \theta - 1)$ , and  $P_3 = (1/2)(5 \cos^3 \theta - 3 \cos \theta)$ , together with  $z = r \cos \theta$  and  $\rho = r \sin \theta$ , we get

$$\psi(\rho, z) = -\frac{1}{2} \mu_0 I_a \left[ \frac{z}{a} - \frac{1}{2} \frac{z^3}{a^3} + \frac{3}{4} \frac{z \rho^2}{a^3} \right].$$

Therefore,

$$B_z = -\frac{\partial \psi}{\partial z} = \frac{\mu_0 I_a}{2a} \left[ 1 - \frac{3}{2} \frac{z^2}{a^2} + \frac{3}{4} \frac{\rho^2}{a^2} \right] = \frac{\mu_0 I_a}{2a} \left[ 1 - \frac{3}{2} \frac{b^2 \cos^2 \theta}{a^2} + \frac{3}{4} \frac{b^2 \sin^2 \theta}{a^2} \right]$$

and

$$B_\rho = -\frac{\partial \psi}{\partial \rho} = \frac{3\mu_0 I_a}{4} \frac{z \rho}{a^3} = \frac{3\mu_0 I_a}{4} \frac{b^2}{a^3} \sin \theta \cos \theta.$$

Substituting these fields into the torque formula and collecting terms gives the advertised result:

$$N_x = \frac{1}{2} \mu_0 I_a I_b \frac{b^2}{a} \int_0^{2\pi} d\theta \left[ \cos^2 \theta \left( 1 - \frac{3b^2}{2a^2} \right) + \frac{15b^2}{16a^2} \sin^2 2\theta \right] = \frac{\pi}{2} \mu_0 I_a I_b \frac{b^2}{a} \left[ 1 - \left( \frac{3b}{4a} \right)^2 \right].$$

### 12.19 Equivalence of Force Formulae

$U_B$  must be expressed as a function of the flux variables.  $\hat{U}_B$  must be expressed as a function of the current variables. To do this, we use

$$\Phi_k = M_{k\ell} I_\ell \quad \text{and} \quad I_k = M_{k\ell}^{-1} \Phi_\ell. \quad (1)$$

Therefore,

$$U_B = \frac{1}{2} \sum_{k=1}^N I_k \Phi_k = \frac{1}{2} \sum_{k=1}^N \Phi_k M_{k\ell}^{-1} \Phi_\ell$$

$$\hat{U}_B = -\frac{1}{2} \sum_{k=1}^N I_k \Phi_k = -\frac{1}{2} \sum_{k=1}^N I_k M_{k\ell} I_\ell.$$

Substituting these expressions into the force formulae in the statement of the problem shows that the proposition will be proved if we can show that

$$\Phi_k \nabla M_{k\ell}^{-1} \Phi_\ell = -I_k \nabla M_{k\ell} I_\ell. \quad (2)$$

We begin with  $\mathbf{M}\mathbf{M}^{-1} = \mathbf{I}$  written in component form:

$$M_{k\ell} M_{\ell p}^{-1} = \delta_{kp}.$$

Using this,

$$(\nabla M_{k\ell}) M_{\ell p}^{-1} + M_{k\ell} (\nabla M_{\ell p}^{-1}) = 0.$$

Multiplying on the right by  $M_{ps}$  and summing over  $p$  gives

$$(\nabla M_{k\ell}) M_{\ell p}^{-1} M_{ps} = -M_{k\ell} (\nabla M_{\ell p}^{-1}) M_{ps}.$$

Using the definition of the inverse,

$$(\nabla M_{k\ell}) \delta_{\ell s} = -M_{k\ell} (\nabla M_{\ell p}^{-1}) M_{ps}.$$

The left side of this equation is  $\nabla M_{ks}$ . Therefore, using (1) and the fact that  $M_{k\ell} = M_{\ell k}$ ,

$$\begin{aligned} -I_k \nabla M_{ks} I_s &= -I_k \left[ -M_{k\ell} (\nabla M_{\ell p}^{-1}) M_{ps} \right] I_s \\ &= I_k M_{k\ell} \nabla M_{\ell p}^{-1} \Phi_p \\ &= M_{\ell k} I_k \nabla M_{\ell p}^{-1} \Phi_p \\ &= \Phi_\ell \nabla M_{\ell p}^{-1} \Phi_p. \end{aligned}$$

This is (2), as required.